

# Designing coils to minimize the maximal induced electrical field amplitude in a patient

Gael Bringout<sup>a,\*</sup>, Johan Löfberg<sup>b</sup>, Patricia Ulloa<sup>a</sup>, Martin A. Koch<sup>a</sup>, Thorsten M. Buzug<sup>a</sup>

<sup>a</sup> Institute of Medical Engineering, Universität zu Lübeck, Germany

<sup>b</sup> Department of Electrical Engineering, Linköping University, Sweden

\* Corresponding author, email: bringout@imt.uni-luebeck.de

**INTRODUCTION** Peripheral nerve stimulation (PNS) due to the electrical field  $\vec{E}$  induced in the patient body limits the increase of the drive field amplitude and thus the imaging field of view (FOV) and speed [1-4]. In order to maximize the drive field amplitude, the minimization of the normalized maximal induced electrical field amplitude (nMIEFA) [5] is done during the design of  $x$ -,  $y$ - and  $z$ -drive coils.

**MATERIAL AND METHODS** The coil design can be formulated as a problem minimizing the dissipated power  $P_{QCQP}$  and constraining the field quality [6], typically called quadratically constrained quadratic program (QCQP). To minimize the nMIEFA, a Second-Order Conic Program (SOCP) problem is introduced and formulated as

$$\min_{\vec{s}} \max_k (\|\vec{E}_k(\vec{s})\|)$$

subject to:  $P_{SOCP} \leq n P_{QCQP}$

with  $\vec{s}$  the surface current density,  $k = 1, \dots, K$  with  $K$  the number of considered surface elements forming the patient model,  $P_{SOCP}$  the dissipated power for the solution and  $n$  an integer equal to 2, 4, 6 or 8. Additionally, the same constraint on the field quality is applied as the one used for the QCQP problem. All problems are solved using the YALMIP toolbox [7] and the MOSEK (7.0, Mosek ApS, Denmark) solver.

The induced electrical field is evaluated according to [8].

A cylindrical surface with a diameter of 0.640 m and a length of 0.4 m is discretised in 400 triangles and is used as support for the coil.

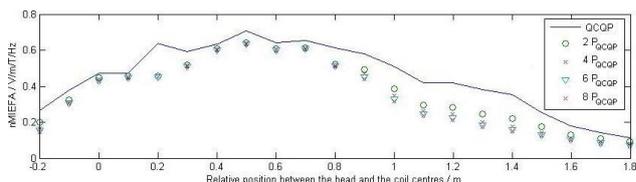
The surfaces of two patients are modelled either from photos or via the segmentation of the body/air interface from a whole body MRI acquired with a voxel size of  $0.8 \times 0.8 \text{ mm}^2$ , a slice thickness of 5 mm and a distance between slices of 5.5 mm. The mesh coming from the MRI acquisition is segmented using 3DSlicer [9]. Both meshes are then post-processed using Meshmixer (v10.7.84, Autodesk Inc, USA) to obtain fully connected meshes.

**RESULTS** The nMIEFA on 2 human models are calculated at 22 different positions for 3 magnetic field topologies and 5 different optimisation problems resulting in 660 optimisations. The results for the optimisation of  $y$ -drive coils in relation with the MRI-based model is presented in Fig. 1. Four surface current densities are shown in Fig. 2, which illustrates the variation of the coils.

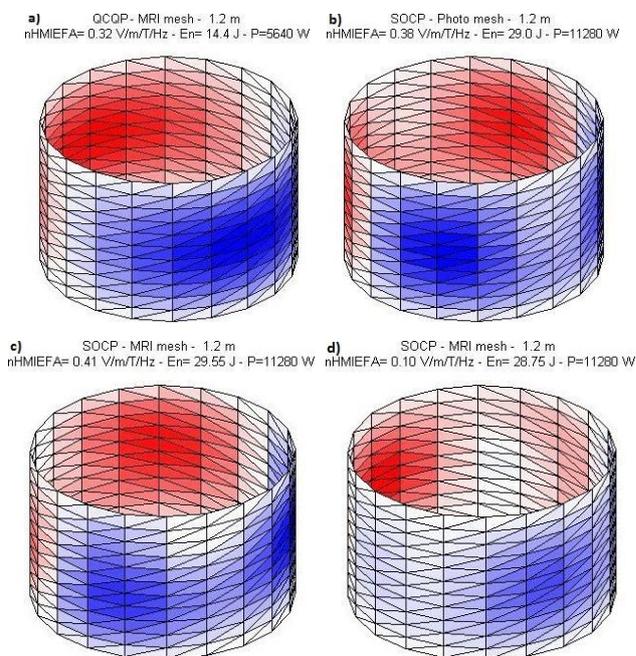
**CONCLUSION** An nMIEFA reduction of up to 50 % for a given position can be expected for a coil optimised to minimize it. This result is patient and position dependent. The technical difficulties associated with such coils may outweigh the reduction of PNS and the increase of FOV.

**ACKNOWLEDGEMENTS** The authors gratefully acknowledge the financial support of the German Federal Ministry of Education and Research (BMBF, grant number 13N11090) and of the European Union

and the State Schleswig-Holstein (Programme for the Future – Economy, grant number 122-10-004).



**Figure 1:** nMIEFA for 5  $y$ -drive coil optimisations on the mesh based on a MRI acquisition of a human subject.



**Figure 2:** Surface current density for  $y$ -drive coils obtained from QCQP (a) and SOCP (b, c, d) problems at position 1.2 m (a, b, c) or 0.5 m (d) from photo (b) and MRI (a, c, d) based meshes.

## REFERENCES

- [1] J. Bohnert. KIT Scientific Publishing, Karlsruhe, 2011.
- [2] G. Bringout et al.. *IWMPi*, 2012. doi: 10.1007/978-3-642-24133-8\_57.
- [3] I. Schmale et al.. *IWMPi*, 2013. doi: 10.1109/IWMPi.2013.6528346.
- [4] E. U. Saritas et al.. *IEEE Transactions on Medical Imaging*, 32(9):1600-1610, 2013. doi: 10.1109/TMI.2013.2260764.
- [5] G. Bringout and T. M. Buzug. 2015 *5th International Workshop on Magnetic Particle Imaging (IWMPi)*. doi: 10.1109/IWMPi.2015.7107077.
- [6] G. Bringout and T. M. Buzug. *IEEE Transactions on Magnetics*, 51(2), 2014. doi: 10.1109/TMAG.2014.2344917.
- [7] J. Löfberg. 2004 *IEEE International Symposium on Computer Aided Control Systems Design*, 2004. doi:10.1109/CACSD.2004.1393890.
- [8] C. C. Sanchez et al.. *Physics in Medicine and Biology*, 55:3087-3100, 2010. doi: 10.1088/0031-9155/55/11/007.
- [9] A. Fedorov et al.. *Magnetic Resonance Imaging*, 30(9):1323-1341, 2012. doi: 10.1016/j.mri.2012.05.001.